



James Mueller Lecture:

"Thermal Barrier Coatings for Gas Turbines"

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Gas Turbines



Fuel Efficiency in the Aeroturbine Industry



Gas Turbines Offer High Power Densities and Route to Quickly Displace Coal



Source: U.S. Energy Information Administration, Form EIA-923, *Power Plant Operations Report.*

Replacing coal with natural gas turbines decreases CO2, Hg, radioactive and dust emissions, and is also more energy efficient.



What 1% Improvement in Gas Turbines Could Buy Us



NB. 30% of natural gas is used to produce electricity. 1% improvement > all renewables

Output Power Depends on Turbine Inlet (T4) Temperature



Dimiduk and Perepezko, MRS Bull 639 2003

Increase in Turbine (T4) Temperatures over Fifty Years



Thermal barrier coatings have enabled a jump in turbine temperatures and energy efficiencies

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 $\sim 150 - 500$ micron thick

Thermal gradient ~ 150-200 K/mm

Thermal Conductivity of Oxides



Kingery et al, ca 1955

Zirconias -- Levi

Thermal conductivity asymptotes to a minimum value at high temperatures

Approach:

Adopt Debye equation and express it's high-temperature limit in terms of measurable physical parameters.

$$\kappa \to \kappa_{\min}$$
; $\kappa = C_V v_m \Lambda / 3 \to k_B v_m \Lambda_{\min}$

Dulong-Petit equation: $C_V \rightarrow 3k_B$ as $T > \Theta_D$

Mean phonon velocity:
$$v_m = 3^{1/3} \left(\frac{1}{v_p^3} + \frac{2}{v_s^3} \right)^{-1/3}$$

Combining these approximations:

$$\kappa_{\min} \to 0.87 k_B N_A^{2/3} \frac{m^{2/3} \rho^{1/6} E^{1/2}}{M^{2/3}}$$
$$\Theta_D = 3.39 \frac{\hbar}{k_B} N_A^{1/3} \frac{m^{1/3} E^{1/2}}{M^{1/3} \rho^{1/6}}$$

$$\Lambda_{\min} \to \left(\frac{M}{\rho \, m \, N_A}\right)^{1/3}$$

Cube root of atom volume

Over wide range of Poisson ratio: $v_m = A \sqrt{\frac{E}{\rho}}$ $A = 0.87 \pm 0.02$

In terms of atomic volume

$$\kappa_{\min} = k_B v_m \Lambda_{\min} \rightarrow 0.87 k_B \overline{\Omega}_a^{-2/3} \left(E / \rho \right)^{1/2}$$

High-Temperature Thermal Conductivity Scaling



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Oxides with Low Conductivity Discovered in Last Decade



Examples of Grain Size Effect

SrTiO3



Tetragonal zirconia

Grain size effect on thermal conductivity can be significant at low temperatures but decreases with increasing temperatures until at highest temperatures there is little or no effect

The Y-Ta-Zr-O System



Pitek and Levi, Surf. & Coatings Tech. 201 (2007) 6044-6050 Phase diagram : Leckie et al. 2010

The $ZrO_2 - YTaO_4$ Pseudo-Binary

Particular interest in compositions along ZrO₂-YTaO₄ Binary

 Y_{1-x}^{3+} Ta⁵⁺_{1-x} Zr⁴⁺_{2x}O²⁻₂ compositions do not require structural vacancies to be stable.

Consequently, no conductivity decrease by oxygen vacancies is possible.

Multi-phase Yttria-Tantala-Zirconia with Low Thermal Conductivity

Variation of Thermal Conductivity with Composition

Limarga et al, J Euro. Ceram Soc, 2014

Obtained by interpolation from conductivity measured at different compositions

Phase Transformations in $(Y,Ta)_{1-x}Zr_xO_{4-2x}$

- YTaO₄ undergoes *reversible* phase transformation, *m t*, in which is, evidently, ferroelastic, involving atomic displacement and twinning, and maybe useful as a high temperature toughening mechanism.
- <u>Effect of ZrO₂ solid solution in YTaO₄ :</u>
- Stabilizes the tetragonal phases, decreasing the *t-m* transformation temperature and increasing the fraction of non-transformable tetragonal phases retained at room temperature
- Solid solution creates mass disorder that decreases the phonon mean free path.
 Evident in:
 - the increase in Raman peaks width
 - the decrease in thermal conductivity
- Suppresses grain growth
- Lower thermal conductivity

Phase Transformation in YTaO₄ : Effect of ZrO₂

NB. Some tetragonal retained

Zr⁴⁺ Stabilizes the high-temperature Tetragonal Phase

The Thermal Management Challenge

Porosity Reduces Conductivity and Scatters Thermal Radiation

Temperature Distribution For Different Coating Designs

Liguo Chen, Phd Thesis

Temperature Distribution For Different Coating Designs

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Basis of Optical Probing of a TBC

TBCs are optically turbid media – highly scattering but are translucent Hence some light can penetrate through to the TGO underneath the TBC

Luminescence Based Temperature and Damage Sensor

Non-contact method

• Luminescent ions can be incorporated into crystal structure of the coating material to act as sensors

• Luminescence lifetime is known to be temperature sensitive

• Because of translucency of TBC materials, visible lasers and luminescence can be used to measure temperatures of sensors buried in a coating

• Multiple sensor layers can be applied to measure the temperature at any depth

Example: Eu Doped TBC Sensor Layer

Superimposition of white light and UV luminescence images D. R. Clarke, Harvard University, Jan 2015

Temperature Sensing Using Luminescence Lifetimes

10000 700 °C Coating Bulk 0.1 1000 Bulk 100 Intesity (a.u.) Lifetime (μs) 10 0.01 1 Coating 1100°C 0.1 700°C 0.01 0.001 600 1200 0 200 400 800 1000 8 2 4 6 0 Time (us) Temperature (⁰C)

10 micron Eu-doped sensor layer in a EB-PVD YSZ coating

Calibration of luminescence lifetime provides basis for temperature measurements on engine components

TBC Interface Temperature in a Thermal Gradient

with D. Zhu and J. Eldridge, NASA Glenn. Surf Coat Tech Vol 201 (2006) D. R. Clarke, Harvard University, Jan 2015

TBC Interface Temperature in a Thermal Gradient

TBC thickness: 146 µm

Effect of Thermal Cycling on Coating Life

SWRI report

Thermal Cycling Instability

Life of TBC is often limited by morphological instability ("rumpling") of the metal bond coat on thermal cycling causing incompatibilities with TBC. More stable alloys needed

Coating surface on thermal cycling. 0-300 cycles to 1150°C in air. ~ 400 micron field of view

TBC Interface after 100 One-hour Cycles to 1150°C

Low magnification

Evolution of Interface Separation Leading to Failure

D. R. Clarke, Harvard University, Jan 2015 Tolpygo, Murphy, Clarke

R-line Luminescence and Piezospectroscopy

Key concepts:

- All alumina contains small (ppm) concentrations of Cr³⁺ in solid solution
- Each Cr³⁺ ion emits photons with an energy dependent on its own local strain environment
- Frequency shift proportional to mean stress in a polycrystalline alumina

$$\Delta v_{R2} = 7.62 \,\sigma_m$$

Basis of Optical Probing of a TBC

TBCs are optically turbid media – highly scattering but translucent Hence some light can penetrate through to the TGO underneath the TBC

Multi-spectral Luminescence Imaging to Reveal Stress Variations

- Illuminate coating with uniform laser beam, 514.3 nm
- Collect R-line luminescence on a CCD through a tunable Fabry-Perot filter
- Tune filter through the luminescence frequency band recording an image at each frequency step
- Invert spectral images to determine R1 shift and hence stress at each image pixel
- Map stress distribution over coating

1.15 – 1.20 GPa

WA12

WA15

1.10 – 1.15 GPa

1.05 – 1.10 GPa

1.00 – 1.05 GPa

0.95 – 1.00 GPa

0.90–0.95 GPa

0.85 – 0.90 GPa

o.80 – o.85 GPa

0.75 – 0.80 GPa

0.70 – 0.75 GPa

0.65 – 0.70 GPa

o.60 – o.65 GPa

0.55 – 0.60 GPa

0.50 – 0.55 GPa

Evolution of Interface Damage with Thermal Cycling

Green areas correspond to areas where the mean stress below 0.7 GPa

Vibrational Damping Due to Oxygen Hopping

Defect Rearrangement Model (Wachman) predicts that damping peak occurs at:

$$T_{p} = \frac{E_{i}}{k_{B} \ln \omega \tau}$$
 Activation energy for hopping

The Next Materials Frontier: Ceramic Matrix Composites

- Higher temperature capability
- High corrosion resistance
- Toughening mechanisms:
 - Microcracking
 - Fiber pull out
 - Crack bridging
- 90% cooling air reduction
- Reduced emissions

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Future Limits To Gas Turbines: Unresolved Challenges

- Atmospheric pollution from engine exhausts
 - Chemical reactions produce NOx -- will limit max combustion temperature

- Melting of ingested sand can erode TBC -- CMAS
- Corrosion of metallic components from pollution in the atmosphere, eg SO₂
 - Many of the metallic alloys in the engine were not designed to resist SO₂ corrosion

NOx Emissions Depend on Combustion Temperature

On land-based turbines, *NOx* can be reduced by steam injection into combustor

Aerospace turbines might need their own high-temperature catalytic convertor

Growing problem: rising SO2 levels in air in many cities around the world Probably will require extensive modification of bond-coat alloys.

SO₂ Corrosion Resistance

Growing problem: rising SO2 levels in air in many cities around the world. Current bond-coat alloys were designed for much lower SO2 levels. Solution: probably will require extensive modification of bond-coat alloys.

Summary and Future Directions

Identifying the next generation thermal barrier coatings remains a major challenge

- Low thermal conductivity at high temperatures is a *necessary but not sufficient* criterion.
- Thermal conductivity at low temperatures is relatively un-important and not a good guide to high-temperature conductivity
- High fracture toughness at high temperatures is also a necessary requirement.
- Thermal barrier coatings are part of a dynamically evolving and interacting system.
- Bond-coat and superalloy must also be morphologically stable, especially on thermal cycling

Future Directions

- Development of *in-situ* monitoring, particularly of coating temperatures and damage.
- Operation in air containing higher SO2 concentrations.
- Coatings for turbines using alternative fuels.
- Plenty of inter-disciplinary research and development opportunities
- Success will require a large scale, multidisciplinary approach and extensive collaborations

- □ Office of Naval Research, Steve Fishman and Dave Shifler
- Uladimir Tolpygo, Andi Limarga, Molly Gentleman, Sam Shian, Yang Shen,
- □ Vanni Lughi, Liguo Chen, Matthew Chambers, John Nychka, Mary Gurak
- Professors Carlos Levi and Tony Evans, UC Santa Barbara
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- Mike Maloney, Pratt and Whitney
- Ram Darolia, GE Aviation, Don Lipkin, GE Corporate Research
- □ Vladimir Tolpygo and Wil Baker, Honeywell Aviation
- Bauke Heeg, Luminium

Want to Know More ?

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Turbine Aerodynamics, Heat Transfer, Materials, and Mechanics

Edited by Tom I-P. Shih Vigor Yang

